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(71) Applicant: UBE-NITTO KASEI CO. LTD.
Chuo-ku Tokyo 103 (JP)

(72) Inventors:

- YOKOKITA, Masahiko,
UBE-NITTO KASEI CO., LTD.
Chuo-ku, Tokyo 103 (JP)
- SHICHIRI, Yoshinobu,
UBE-NITTO KASEI CO., LTD.
Chuo-ku, Tokyo 103 (JP)

- ONODERA, Akio,
UBE-NITTO KASEI CO., LTD.
Chuo-ku, Tokyo 103 (JP)
- WATANABE, Toru,
UBE-NITTO KASEI CO., LTD.
Chuo-ku, Tokyo 103 (JP)
- MATSUNO, Shigehiro,
UBE-NITTO KASEI CO., LTD.
Chuo-ku, Tokyo 103 (JP)

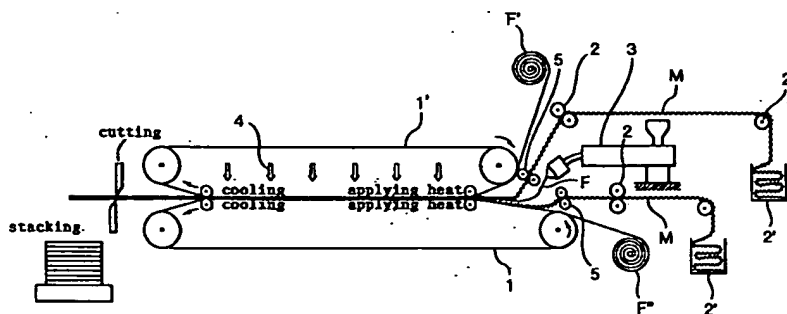
(74) Representative: Klingseisen, Franz, Dipl.-Ing.
Patentanwälte,
Dr. F. Zumstein,
Dipl.-Ing. F. Klingseisen,
Postfach 10 15 61
80089 München (DE)

(54) **GLASS FIBER MAT FOR STAMPABLE SHEET, PROCESS FOR THE PRODUCTION OF THE MAT, STAMPABLE SHEET MADE FROM SAID MAT, PROCESS FOR THE PRODUCTION OF THE SHEET, AND EQUIPMENT FOR THE PRODUCTION THEREOF**

(57) A glass fiber mat for a stampable sheet, in which long fiber and short fiber may not separate even by forming and both are distributed uniformly to make features of respective fibers effective. A production system includes a double belt press type laminator which stacks the glass fiber mat, a thermoplastic resin melt and a film which is taken up and applies heat and pressure for impregnation, and cools with maintaining a condition applied the pressure, supply means for supplying

the glass fiber mat into said laminator, and a pair of pressure shearing rollers arranged between the supply means and an endless belt of said laminator for partially cutting the glass fiber into short fiber. The roller is made of steel to apply line pressure on to the glass fiber mat to shear the continuous fiber to uniformly distribute short fiber in long fiber.

FIG.1



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Description

APPLICABLE FIELD OF THE INVENTION

5 The present invention relates to a glass fiber mat for a stampable sheet, a production process thereof, a stampable sheet employing the glass fiber mat, a production process thereof, and a production system therefor.

BACKGROUND OF THE INVENTION

10 A stampable sheet is a sheet form article, in which a thermoplastic resin is impregnated in a reinforcement fiber. There are various stampable sheets depending upon production processes, forms of reinforcement fibers. As production processes of the stampable sheet, a lamination method and dispersing method have been known.

15 The lamination method is a method, in which a fiber mat is prepared from the reinforcement fiber at first, the fiber mat and a thermoplastic resin sheet or molten thermoplastic resin sheet are stacked, and then, the thermoplastic resin is impregnated into the fiber mat by applying heat and pressure (U. S. Patents Nos. 3,644,909, 3,713,962 and 3,850,723).

20 On the other hand, the dispersing method is a method for producing the stampable sheet, in which after mixing to disperse reinforcement fiber and thermoplastic resin, the mixture is shaped into a sheet form, and heat and pressure is applied to the sheet form mixture, which is divided into a wet method to perform mixing and dispersing in water (Japanese Examined Patent Publication (Kokoku) No. Heisei 2-48423, Japanese Examined Patent Publication No. Heisei 3-4678 and Japanese Examined Patent Publication No. Heisei 4-40372) and a dry method to perform mixing and dispersing within a special mixer without using water (Japanese Examined Patent Publication No. Heisei 3-55312, Japanese Examined Patent Publication No. Heisei 2-42058 and Japanese Unexamined Patent Publication (Kokai) No. Heisei 4-173311). The wet method is to mix reinforcement short fiber and thermoplastic resin powder in water, make into a sheet
 25 by a paper machine with adding a flocculating agent or a binder, remove water and dry to form a sheet, stack a plurality of sheets as required, and apply heat and pressure to obtain the stampable sheet. On the other hand, the dry method is to mix reinforcement fiber and thermoplastic resin powder within a special mixing chamber, to form into sheet form on a belt and to apply heat and pressure to form the stampable sheet.

30 The features of the stampable sheet formed by the lamination method are to have high impact strength since the reinforcement fiber is continuous fiber, and to be difficult to cause local orientation for mechanical entangling of fibers. On the other hand, since the reinforcement fiber cannot be sufficiently filled in a rib or a boss, designed strength cannot be achieved. Therefore, freedom in designing of the product is low.

35 On the other hand, the stampable sheet produced by dispersing method has shorter fiber in comparison with the lamination method to easily cause fluctuation of strength due to local orientation of the reinforcement fiber, and has low impact strength. On the other hand, since the reinforcement fiber can be filled even in the rib or boss, designing of the product is easy.

Therefore, there are several proposals for taking the feature of the short fiber reinforcement in the stampable sheet of the long fiber reinforcement typically as formed by lamination method.

40 For example, examples of attempts for improvement by impregnating a resin containing short fiber in a long fiber mat have been disclosed in Japanese Unexamined Patent Publication No. Showa 48-80172, Japanese Unexamined Patent Publication No. Showa 54-21476, Japanese Unexamined Patent Publication No. Showa 55-161618, Japanese Unexamined Patent Publication No. Showa 57-100029 and Japanese Examined Patent Publication No. Heisei 4-65854. However, in such method, as pointed out in Japanese Unexamined Patent Publication No. Showa 64-4320, most of the short fiber is filtered by the long fiber mat to penetrate almost only resin into the mat. Then, most of the short fiber forms
 45 a layer in the vicinity of the surface of the long fiber mat. When stamp forming is performed with such stampable sheet, the short fiber may occupy most proportion of the reinforcement fiber to be filled, in the rib, boss and the end portion of the formed product, conversely, in a charge portion of the original sheet, the long fiber may occupy most proportion. As a result, difference of proportions of the long fiber and the short fiber can be caused at various portions of the product to cause difference in impact strength and fatigue characteristics, or, anisotropy may be caused due to local orientation
 50 of the short fiber. Furthermore, distortion may also be caused.

While not directed to the stampable sheet, as a sheet form material of a fiber reinforced thermoplastic resin, which can be formed by a pressure forming, and in which the long fiber and the short fiber are combined, there is one, in which a long fiber mat and a short fiber mat are stacked and the thermoplastic resin is impregnated into the stacked mats, as disclosed in Japanese Unexamined Patent Publication No. Showa 58-98241. In this publication, respective one long
 55 fiber mat and short fiber mat are stacked and the thermoplastic resin is impregnated thereinto. With taking this as hint, it can be considered that the stampable sheet, in which the continuous fiber and the short fiber are uniformly distributed can be easily obtained by stacking a plurality of thin continuous fiber mats and thin short fiber mats and formed into a mat by needle punch, and impregnating thermoplastic resin into the needle punched mat. However, when this is practiced, as shown in Fig. 7, for example, production units (A) of the continuous fiber mat and production units (B) of the

short fiber mat have to be arranged alternately along transporting direction (left and right direction in the drawing) of a conveyer C and thus requires a huge amount of investment.

Then, upon needle punching the continuous fiber mat, when punching density is increased or penetration depth of the needle is made deeper, cutting of the fiber is increased. Thus, a mat, in which the short fiber is distributed in the continuous fiber, can be obtained. By impregnating the thermoplastic resin in this mat, the stampable sheet can be obtained.

However, such stampable sheet holds the following drawback. Namely, when the punching density is increased, entangling of the fibers can become stronger to make the mat difficult to loose upon forming. This causes requirement for higher forming pressure. On the other hand, when the penetration depth of the needle is made deeper, the fibers oriented in the thickness direction is increased to make a loft (nominal thickness) of the mat larger. As a result, upon heating, a blank (hot blank) is expanded significantly to cause temperature difference between the inner layer and the surface layer. If heating period is expanded for eliminating the temperature difference, the surface layer can be over-heated to degrade appearance. Furthermore, heating aging can be promoted to degrade physical properties.

Therefore, the present invention is to provide a glass fiber mat for a stampable sheet, in which long fiber and short fiber may not be separated and distributed uniformly even in forming process, and which can make features in respective fiber effective, a production process thereof, a stampable sheet employing this glass fiber mat, a production process thereof, and a production system therefor.

SUMMARY OF THE INVENTION

As a result of extensive study for solving the problems set forth above, the inventor has found that the problem can be solved by employing a glass fiber mat, in which a glass fiber mat forming a glass fiber mat for a stampable sheet is formed with continuous glass fiber and short glass fiber produced by clamping the glass fiber under pressure for partially causing cutting of the fiber, and thus containing long fiber in the length longer than or equal to 10 mm and short fiber in the length shorter than 10 mm.

In the preferred construction, the glass fiber mat is obtained by clamping a continuous fiber needling mat, in which different fiber length of fibers are entangles each other, and the long fiber having fiber length greater than or equal to 10 mm and short fiber having fiber length less than 10 mm are distributed uniformly. The glass fiber mat may contains 30 to 60 Wt% of glass fiber having fiber length less than 10 mm, 70 to 40 Wt% of glass fiber having fiber length greater than or equal to 10 mm, and the glass fiber having fiber length greater than or equal to 10 mm contains more than or equal to 5% of glass fiber having fiber length greater than or equal to 50 mm. When a unit weight is 900 g/m², a tensile strength is 0.5 to 3 kgf/200 mm and a mat loft is 5 to 10 mm.

A stampable sheet, according to the present invention, is produced by impregnating a thermoplastic resin into the glass fiber mat. Preferably, a fiber content is 40 Wt% and a unit weight is 4.4 kg/m², a hot blank loft is 6 to 16 mm.

A production process for producing a glass fiber mat to be formed into a fiber reinforced thermoplastic resin stampable sheet by impregnation of a thermoplastic resin, according to the present invention, comprises a step of clamping a glass fiber mat formed with continuous glass fiber or a continuous glass fiber needling mat between a pair of rollers at a predetermined pressure to form long fiber having fiber length greater than or equal to 10 mm and short fiber having fiber length less than 10 mm which are formed by partially cutting the glass fiber.

A production process for producing a fiber reinforced thermoplastic stampable sheet by impregnating a thermoplastic resin, according to the present invention, comprises the steps of needling a continuous glass fiber mat for entangling fibers, clamping the glass fiber mat formed with continuous glass fiber for partially cutting the fiber, and thereafter impregnating the thermoplastic resin.

A production system of a stampable sheet, according to the present invention, comprise a laminator, fiber mat supply means for supplying a glass fiber mat into the laminator, and a pair of rollers arranged between the laminator and the fiber mat supply means and clamping the fiber mat for partially cutting the glass fiber into longer fiber having fiber length greater than or equal to 10 mm and short fiber having fiber length less than 10 mm.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is an explanatory illustration showing one embodiment of a stampable sheet producing system according to the present invention;

Fig. 2 is a perspective view showing a sample for deriving a minimum forming pressure;

Fig. 3 is a perspective view showing a sample for evaluating forming mobility A (GC ratio);

Fig. 4 is a perspective view showing a sample for measuring general mechanical property;

Fig. 5(a) is a perspective view showing a sample for evaluating forming mobility B (flow of GF to a rib), Fig. 5(b) is an enlarged section of the rib;

Fig. 6 is a perspective view showing a sample for evaluation of anisotropy; and

Fig. 7 is an explanatory illustration showing one example of the conventional production process of a composite

mat of continuous fiber and short fiber.

DESCRIPTION OF THE PREFERRED EMBODIMENT

A glass fiber mat, in accordance with the present invention, is constructed with a glass fiber mat forming a glass fiber mat for a stampable sheet formed with continuous glass fiber and short glass fiber produced by clasping the glass fiber under pressure for partially causing cutting of the fiber, and thus contains long fiber in the length longer than or equal to 10 mm and short fiber in the length shorter than 10 mm.

Here, it is preferred that the short fiber (fiber length is less than 10 mm) and the long fiber (fiber length is greater than or equal to 10 mm) are distributed uniformly in the mat. While a construction, in which short fiber is arranged on upper and lower surfaces of a mat of the long fiber can be often seen, the short fiber and the long fiber may be separated in secondary forming to cause local concentration in the length of the fiber to be filled in various portions of the formed product. This can be a cause of fluctuation of mechanical property to make difficulty designing of the products.

It is preferred that the glass fiber having the fiber length greater than or equal to 10 mm is contained in a rate of 40 to 70 Wt%. In case of the mat having only fiber less than 10 mm of the fiber length, the stampable sheet obtained from such mat has poor impact resistance and is easily cause local orientation of the fiber during forming. On the other hand, in case of the glass fiber mat formed with fiber having a fiber length greater than or equal to 10 mm, number of entangling points becomes large number to require higher forming pressure for obtaining secondary product. As a result, low productivity such as forming speed can be lowered and large scale of production facility becomes necessary.

On the other hand, it is further preferred that the glass fiber having fiber length greater than or equal to 50 mm is contained in a range of 5 to 10 Wt%. When the content of the glass fiber having fiber length greater than or equal to 50 mm is less than 5%, the short fiber and the longer fiber may be separated during secondary forming to local concentration of the fiber, and orientation of the shorter fiber can be caused. As a result, anisotropy in the physical property can be caused. Conversely, when the content of the glass fiber having fiber length greater than or equal to 50 mm is greater than 10%, mobility in the secondary forming tends to be degraded.

On the other hand, in the glass fiber mat, when the unit weight (hereinafter referred to as "Metsuke") is standard 900 g/m², it is preferred that a tensile strength is 0.5 to 3 kgf/200 mm, and a mat loft is 5 to 10 mm. Normally, while the tensile strength of the continuous fiber mat obtained by needling is in the order of 20 kg, most of the fiber is continuously entangled. Thus, it is difficult to fill the glass fiber in the small portion of the formed product, such as rib, boss or so forth. Accordingly, in order to obtain sufficient mobility as intended by the present invention, it is required that the tensile strength is less than or equal to 3 kg. Furthermore, when the tensile strength of the mat is less than 0.5 kg, due to lack of binding power of the mat per se, the mat may easily cause pulling apart or so forth upon transporting a hot blank into a mold. Therefore, it is difficult to use in the light of handling.

The glass fiber mat having the property set forth above can be easily obtained by clasping the needled glass fiber mat. By needling, the continuous fiber entangles to form a mat which can be handled. At this time, by cutting of the fiber, short fiber may be created. However, the proportion of the short fiber thus created is small. Therefore, there is a method shearing of fiber is increased upon needle punching of the continuous fiber mat, by increasing punching density or by increasing penetration depth of the needle, the mat containing large amount of short fiber in the continuous fiber can be obtained.

However, when the punch density is increased, entangling of fiber is strengthened to cause necessity of high forming pressure for difficulty of losing of mat in secondary forming. On the other hand, when the penetration depth of the needle is increased, fiber oriented in the thickness direction of the mat is increased to make mat loft (nominal thickness) greater. As a result, blank (hot blank) is significantly expanded to cause temperature difference between the inner layer and the surface layer in the blank. When heating period is expanded for eliminating the temperature difference, the surface layer becomes overheating condition to cause degradation of the external appearance of the formed product. Also, thermal aging is promoted to degrade physical property.

By clasping the needled glass mat as in the present invention, the entangled portion is selectively compressed and cut, wide range of fiber length distribution can be provided for reducing mat loft which can be a problem during heating.

As a method of clasping according to the present invention, it is simply apply pressure by clamping the glass fiber mat between two metal plates. For continuous production, it is desirable to clamp the glass fiber mat with a pair of metal rolls. On the other hand, by providing unevenness of the metal plates or roll, the mat with partially cut fiber can be obtained.

The hot blank loft of the stampable sheet according to the present invention is preferably 6 to 16 mm, and more preferably 8 to 12 mm. When the hot blank loft is less than 6 mm, the surface of the molten stampable sheet becomes tackiness can easily cause adhesion of the resin on a working glove during transportation of material to lower handling ability. On the other hand, when the hot blank loft is greater than or equal to 16 mm, heat mark (temperature difference) can be caused in the surface layer and the intermediate layer to cause lowering of mobility.

In the glass fiber mat according to the present invention, the standard mat loft, in which the Metsuke is 900 g/m², is preferably 5 to 10 mm, and more preferable 6 to 8 mm. When the mat loft is less than 5 mm, the resin may locally

concentrated on the surface layer of the stampable sheet blank in resin impregnation process by lamination, and as a result, influence for handling, such as surface tackiness or so forth during heated state (hot blank) in secondary forming. Conversely, in case of the mat loft greater than or equal to 10 mm, the hot blank loft can become greater than or equal to 16 mm upon processing of the stampable sheet to cause heating mark.

EXAMPLES 1 TO 4, COMPARATIVE EXAMPLES 1 TO 3

With employing glass fiber roving (manufactured by Nitto Boseki K.K.) shown in a table 1, after shaking off the glass fiber roving without providing directionality, needle punching was effected under the condition of punching density of 30 needles/cm² and penetration depth of the needle of 14.5 mm to obtain the glass fiber mat of Metsuke 900 g/cm². This glass fiber mat was supplied to a stampable sheet producing system shown in Fig. 1 to obtain the stampable sheet of 40 Wt% of glass content, 4.4 kg/m² of Metsuke.

The stampable sheet producing system includes a double belt press type laminator 4 which laminates the supplied glass fiber mat with the thermoplastic resin melt F and thermoplastic resin films F' and F" wound on rolls, impregnates the resin by applying heat and pressure, cools the resin impregnated laminate under pressure to form into a sheet, a supply means for supplying the glass fiber mat M to the laminator, and a pair of pressure shearing rollers 5 located between the supply means 2 and endless belts 1, 1' of the laminator 4 for clamping the glass fiber mat to cut a part of fibers into short fiber. The roller is made of copper and has 200 mm ϕ of diameter, which exerts a line pressure shown in the table 1 for pressure shearing the continuous fiber to uniformly distribute the short fiber in the long fiber.

The pressure shearing line pressure of the roller 5 is set in consideration of the fiber length distribution after process, a mat strength and hot blank loft. This pressure is differentiated depending upon the binder composition or fiber diameter in the roving employed as the glass fiber mat. In order to obtain the glass fiber mat and the stampable sheet according to the present invention, the mat tensile strength and the hot blank loft have to be set within a specific range. For example, in case of the example 1, the pressure shearing line pressure is preferably 60 to 120 kg/cm, and more preferably 80 to 100 kg/cm.

TABLE 1

No.	Name of Roving	Fiber Diameter	Binder	Pressure Shearing Line Pressure	Reinforcement
Exam. 1	RS42RA-305	23 μ m	vinyl acetate	90 kg/cm	Sheared
Comp. 1	RS42RA-305	23 μ m	vinyl acetate	0 kg/cm	Continuous
Exam. 2	RS24QA-305	17 μ m	acryl	35 kg/cm	Sheared
Comp. 2	RS24QA-305	17 μ m	acryl	10 kg/cm	Sheared
Exam. 3	RS24QA-305	17 μ m	acryl	45 kg/cm	Sheared
Exam. 4	RS24QA-305	17 μ m	acryl	70 kg/cm	Sheared
Comp. 3	RS24QA-305	17 μ m	acryl	90 kg/cm	sheared
Comp. 4	RS24QA-305	17 μ m	acryl	0 kg/cm	continuous/chopped
Comp. 5	RS24QA-305	23 μ m	vinyl acetate	45 kg/cm	Sheared
Comp. 6	RS24QA-305	23 μ m	vinyl acetate	135 kg/cm	Sheared
Comp. 7	RS24QA-305	23 μ m	vinyl acetate	0 kg/cm	Continuous

COMPARATIVE EXAMPLE 4

With employing glass fiber roving (manufactured by Nitto Boseki K.K.) shown in a table 1, after shaking off the glass fiber roving on the conveyer without providing directionality, needle punching was effected under the condition of punching density of 30 needles/cm² and penetration depth of the needle of 14.5 mm to obtain the glass fiber mat of Metsuke 450 g/cm². This glass fiber mat was supplied to a stampable sheet producing system shown in Fig. 1 to obtain the stampable sheet without performing pressure shearing. At this time, for polypropylene to be used as the thermoplastic resin melt F, 33 Wt% of glass chopped strand was added. The polypropylene melt with glass chopped strand was supplied together with films F' and F" of sole polypropylene wound on the rolls (Metsuke 450 g/m²) to obtain the stampable sheet

reinforced by both of the continuous fiber and the short fiber of 40 Wt% of glass content (continuous fiber : glass chopped strand = 50 : 50), 4.4 kg/m² of Metsuke.

COMPARATIVE EXAMPLES 5, 6, 7

With employing glass fiber roving (manufactured by Nitto Boseki K K.) shown in a table 1, after shaking down the glass fiber roving onto the conveyer without providing directionality, needle punching was effected under the condition of punching density of 30 needles/cm² (40 needles/cm² in case of comparative example 7) and penetration depth of the needle of 14.5 mm to obtain the glass fiber mat of Metsuke 900 g/cm². This glass fiber mat was supplied to a stampable sheet producing system shown in Fig. 1 to obtain the stampable sheet with pressure shearing at 0 kg/cm, 45 kg/cm and 135 kg/cm.

EVALUATION METHOD

Properties of the foregoing glass mats for stampable sheet produced under the foregoing conditions are evaluated in the following evaluation method. The results of evaluation is shown in a table 2.

TABLE 2

		Ex. 1	Comp. 1	Comp. 5	Comp. 6	Comp. 7
	Needle Punch Condition (needles/cm ²)	30	30	30	30	40
	Pressure Shearing Condition (kg/cm)	90	NO	45	135	NO
Fiber Length Distribution	less than 10 mm	51	4	18	63	31
	10 to less than 50 mm	42	3	31	37	59
	50 mm or more	7	93	51	0	10
	(Wt%) Total	100	100	100	100	100
	Mat Loft (mm)	7	10	9	4	13
	Mat Strength (kg/200 cm width)	0.8	24.0	3.6	0.4	6.2
	Hot Blank Loft (mm)	10	16	12	6	24

① Mat Strength

From arbitrary position on the clasped glass fiber mat, 6 test pieces of 200 mm in width and 250 mm in length were cut. Employing a universal testing machine, maximum tensile strength was obtained by applying tension at testing speed of 20 mm/min.

② Fiber Length

From the clasped glass fiber mat, fibers were carefully drawn out by pincette and the lengths were read from a scale. The fiber lengths were measured for 1000 fibers per one test piece.

③ Hot Blank Loft

Blanks of 125 mm x 200 mm was heated for about 6 minutes until the surface temperatures became 210 ± 10 °C by a heating furnace set at 320 °C. The heated blank (hot blank) was quickly put on a machine platen. Also, in order to prevent waving in the hot blank, an iron plate of 125 mm x 200 mm (1.6 mm in thickness and 310g in weight) was mounted. After cooling for 1 hour, a weight of 5 kg was further mounted. Then, height at four corners were measured to taken an average thereof as the hot blank loft.

④ Minimum Forming Pressure (How Small Pressure is Required for Forming)

As an indicia of mobility in forming, three boxes shown in Fig. 2 were formed. Pressure in ton, at which two of three

boxed could be formed without wane, was obtained per unit of 5 tons.

Blank Dimension: 125 mm x 200 mm x 3 pieces (330 ± 5g)
 Heating Temperature: 210 ± 10 °C
 5 Press Speed: 12 mm/sec.
 Mold Temperature: 40 °C
 Pressure Holding Period: 15 sec.

⑤ Mobility in Forming A (glass fiber content ratio between charge portion and end portion (hereinafter abbreviated as "GC ratio").

The formed product shown in Fig. 2 was formed at a pressure of 100 tons. Then, GC at the bottom portion and the end portion of the formed product as shown as hatched portion were measured.

$$A = (\text{end portion GC}/\text{bottom portion GC}) \times 100 [\%]$$

⑥ Mechanical Property

The five formed products shown in Fig. 4, having bending strength (ASTM D-790, kgf/mm²) and tensile strength (ASTM D-638, kgf/mm²) at a pressure of 100 tons. From the bottom portions, test pieces are cut as shown in Fig. 4 (10 pieces in average) and measurement was performed with respect to thereto.

⑦ Mobility in Forming B (mobility of glass fiber into the rib)

The formed products shown in Figs. 5(a) and 5(b) are formed under the following conditions and then mobility of the glass fiber into a center rib was evaluated.

Blank Dimension: 143 mm x 333 mm x 2 pieces (420 ± 6g)
 Rib Thickness: 2mm
 30 Rib Height: 20 mm
 Heating Temperature: 210 ± 10 °C
 Press Speed: 16 mm/sec.
 Mold Temperature: 50 °C
 Pressure Holding Period: 30 sec.
 35 Forming Pressure: 180 tons

$$B = (\text{rib tip end GC}/\text{bottom portion GC}) \times 100 [\%]$$

⑧ Anisotropy (It is not desirable to cause strong anisotropy due to orientation of GF at the flowing portion)

The formed product shown in Fig. 6 was formed under the following condition. Then, bending properties at the bottom portion, longer side portion and shorter side portion are evaluated by measuring bending strengths in orthogonal two directions and expressing the ratio by %.

Blank Dimension: 143mm x 215mm x 4 pieces (541 ± 8 g)
 Heating Temperature: 210 ± 10 °C
 Press Speed: 16 mm/sec.
 50 Mold Temperature: 50 °C
 Pressure Holding Period: 30 sec.
 Forming Pressure: 180 tons

Next, by impregnating polypropylene resin in this mat, stampable sheet was prepared. Property of the obtained stampable sheet was evaluated by the foregoing evaluation methods. The results of evaluation is shown in a table 3.

TABLE 3

	EX.1	COM.1	EX.2	COM.2	EX.3	EX.4	COM.3	COM.4	COM.5	COM.6	COM.7
Hot Blank Loft	10	16	13	17	10	8	8	5	12	6	24
Tensile Strength	8.0	8.7	6.8	8.0	7.3	6.8	5.0	4.7	8.0	6.0	5.8
Bending Strength	14.6	16.8	14.2	16.1	14.9	12.7	11.7	9.9	15.1	12.5	13.7
Minimum Forming Pressure	40	55	30	55	35	25	25	25	45	25	60
Forming Mobility A	96	75	97	80	92	104	103	99	91	100	98
Forming Mobility B	60	6	68	20	74	85	90	87	34	86	67
Anisotropy	109	96	109	101	103	105	106	65	-	-	-
	98	111	100	116	102	98	109	116	-	-	-
	99	105	98	103	99	100	102	153	-	-	-

As can be clear from the table 3, the stampable sheet employing the pressured and sheared mat can lower minimum forming pressure with minimizing lowering of the mechanical strength. Since the glass fiber can flow even into the tip end of the rib or the end portion of the formed product, strength may not lower locally, and significant anisotropy may

not be caused, Furthermore, distortion to be caused on the formed product is small. Therefore, freedom in designing of product can be increased.

It should be noted the foregoing embodiments have been exemplified the preferred range of the tensile strength and the mat loft in the case where Metsuke of the glass mat is 900 g/m^2 . However, even if Metsuke is less than or more than 900 g/m^2 , it should be encompassed within a technical scope of the present invention as long as the reduced values of the tensile strength and the mat loft to Metsuke 900 g/m^2 fall within the foregoing range.

As set forth above, in the glass fiber mat for the stampable sheet according to the present invention, the continuous glass fiber, and long fiber having the fiber length greater than or equal to 10 mm and short fiber having the fiber length less than 10 mm which are formed by partially cutting the continuous glass fiber by clasping, are contained uniformly. Therefore, it may not expand significantly even upon heating so that the temperature difference between the surface layer and the inner layer may not be caused. Also, the obtained formed product has high dimensional stability and small fluctuation of strength and anisotropy so that the stampable sheet having advantages of the long fiber reinforcement and the short fiber reinforcement.

In the production process of the glass mat according to the method of the present invention, since the long fiber having the fiber length greater than or equal to 10 mm and the short fiber having the fiber length less than 10 mm are formed by partially cutting the glass fiber by clasping the glass fiber mat which is formed with continuous glass fiber, at a predetermined pressure, the glass fiber mat suitable for producing superior stampable sheet can be produced while production method is simple.

The production system according to the present invention can produce the glass fiber mat, from which the superior stampable mat can be obtained with simple construction, in which only a pair of rollers are provided between the continuous fiber mat supply means and the laminator.

Claims

1. A glass fiber mat, from which a fiber reinforced thermoplastic resin stampable sheet is produced, containing continuous glass fiber, and long fiber having fiber length greater than or equal to 10 mm and short fiber having fiber length less than 10 mm which are formed by partially cutting said glass fiber by clasping.
2. A glass fiber mat for a stampable sheet as set forth in claim 1, wherein different fiber length of fibers obtained by clasping a continuous fiber needling mat, and the long fiber having fiber length greater than or equal to 10 mm and short fiber having fiber length less than 10 mm are distributed uniformly.
3. A glass fiber mat for a stampable sheet as set forth in claim 1 or 2, which contains 30 to 60 Wt% of glass fiber having fiber length less than 10 mm, 70 to 40 Wt% of glass fiber having fiber length greater than or equal to 10 mm, and said glass fiber having fiber length greater than or equal to 10 mm contains more than or equal to 5% of glass fiber having fiber length greater than or equal to 50 mm.
4. A glass fiber mat for a stampable sheet as set forth in any one of claims 1 to 3, wherein when a unit weight is 900 g/m^2 , a tensile strength is 0.5 to 3 kgf/200 mm and a mat loft is 5 to 10 mm.
5. A stampable sheet produced by impregnating a thermoplastic resin into a glass fiber mat for a stampable sheet as defined in any one of claims 1 to 4.
6. A stampable sheet as set forth in claim 5, wherein when a fiber content is 40 Wt% and a unit weight is 4.4 kg/m^2 , a hot blank loft is 6 to 16 mm.
7. A production process for producing a glass fiber mat to be formed into a fiber reinforced thermoplastic resin stampable sheet by impregnation of a thermoplastic resin comprising a step of clasping a glass fiber mat formed with continuous glass fiber between a pair of rollers at a predetermined pressure to form long fiber having fiber length greater than or equal to 10 mm and short fiber having fiber length less than 10 mm which are formed by partially cutting said glass fiber.
8. A production process for producing a glass fiber mat to be formed into a fiber reinforced thermoplastic resin stampable sheet by impregnation of a thermoplastic resin comprising steps of needling a continuous fiber glass fiber mat for entangling fibers and thereafter clasping said glass fiber mat formed with continuous glass fiber between a pair of rollers at a predetermined pressure to form long fiber having fiber length greater than or equal to 10 mm and short fiber having fiber length less than 10 mm which are formed by partially cutting said glass fiber.
9. A production process for producing a fiber reinforced thermoplastic stampable sheet by impregnating a thermo-

plastic resin comprising the steps of needling a continuous fiber glass fiber mat for entangling fibers, claspings said glass fiber mat formed with continuous glass fiber for partially cutting the fiber, and thereafter impregnating said thermoplastic resin.

5 10. A production system of a stampable sheet comprising:

a laminator;

fiber mat supply means for supplying a glass mat into said laminator; and

10 a pair of rollers arranged between said laminator and said fiber mat supply means and claspings said fiber mat for partially cutting said glass fiber into longer fiber having fiber length greater than or equal to 10 mm and short fiber having fiber length less than 10 mm.

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FIG.1

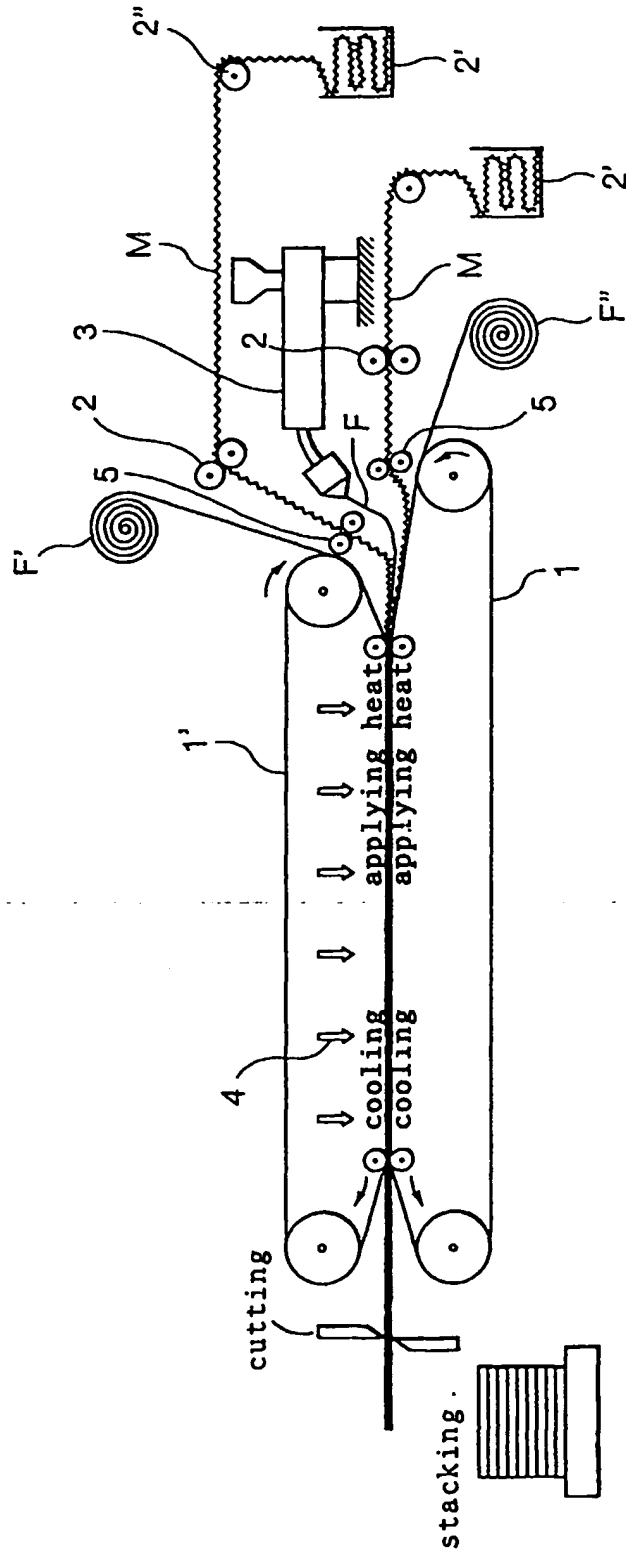


FIG.2

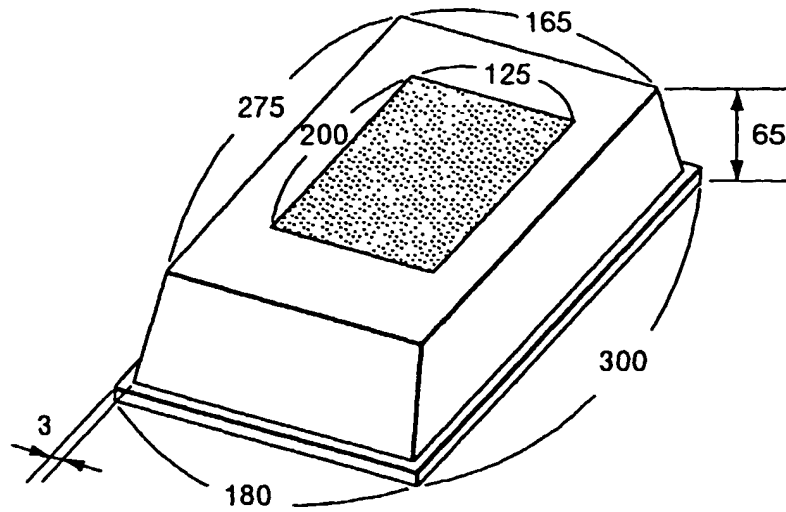


FIG.3

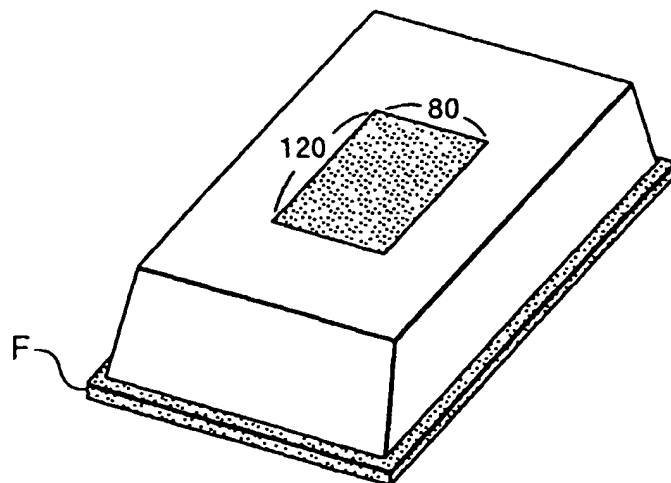


FIG.4

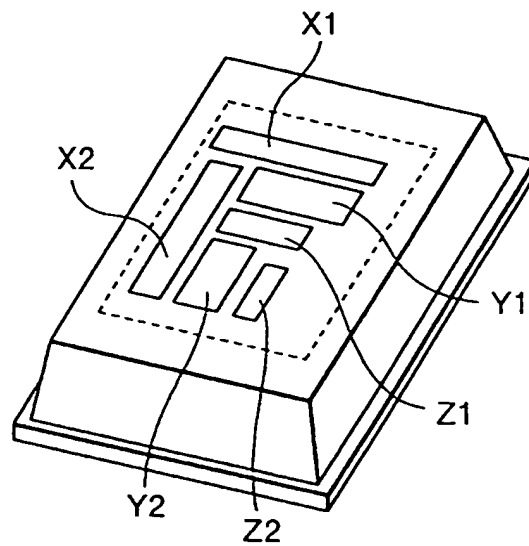
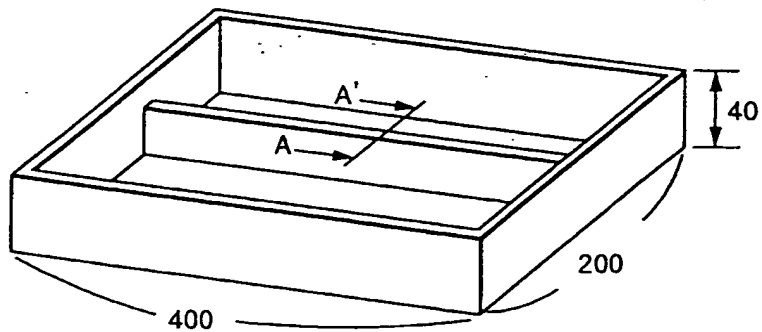


FIG.5

(a)



(b)

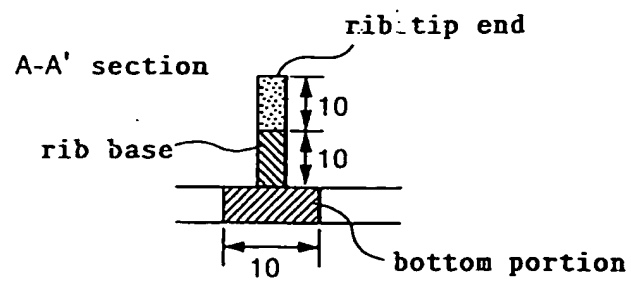


FIG.6

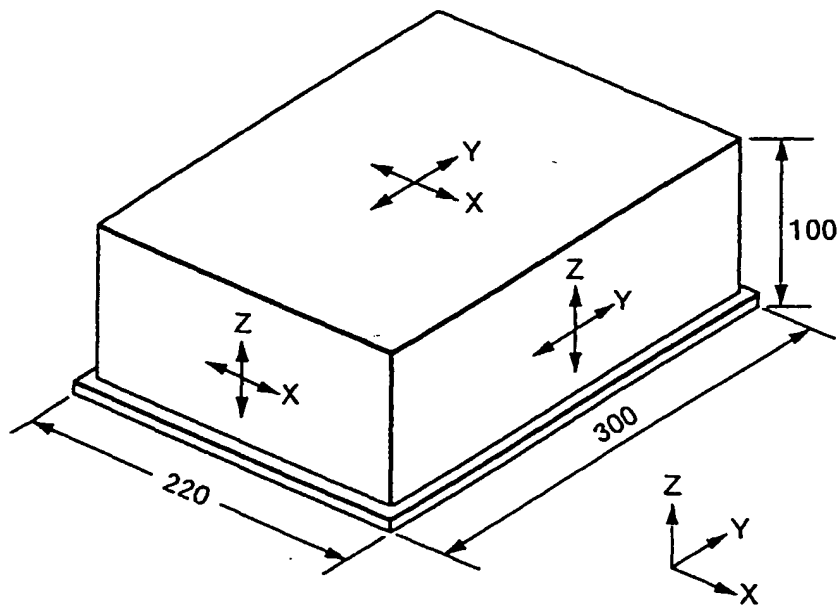
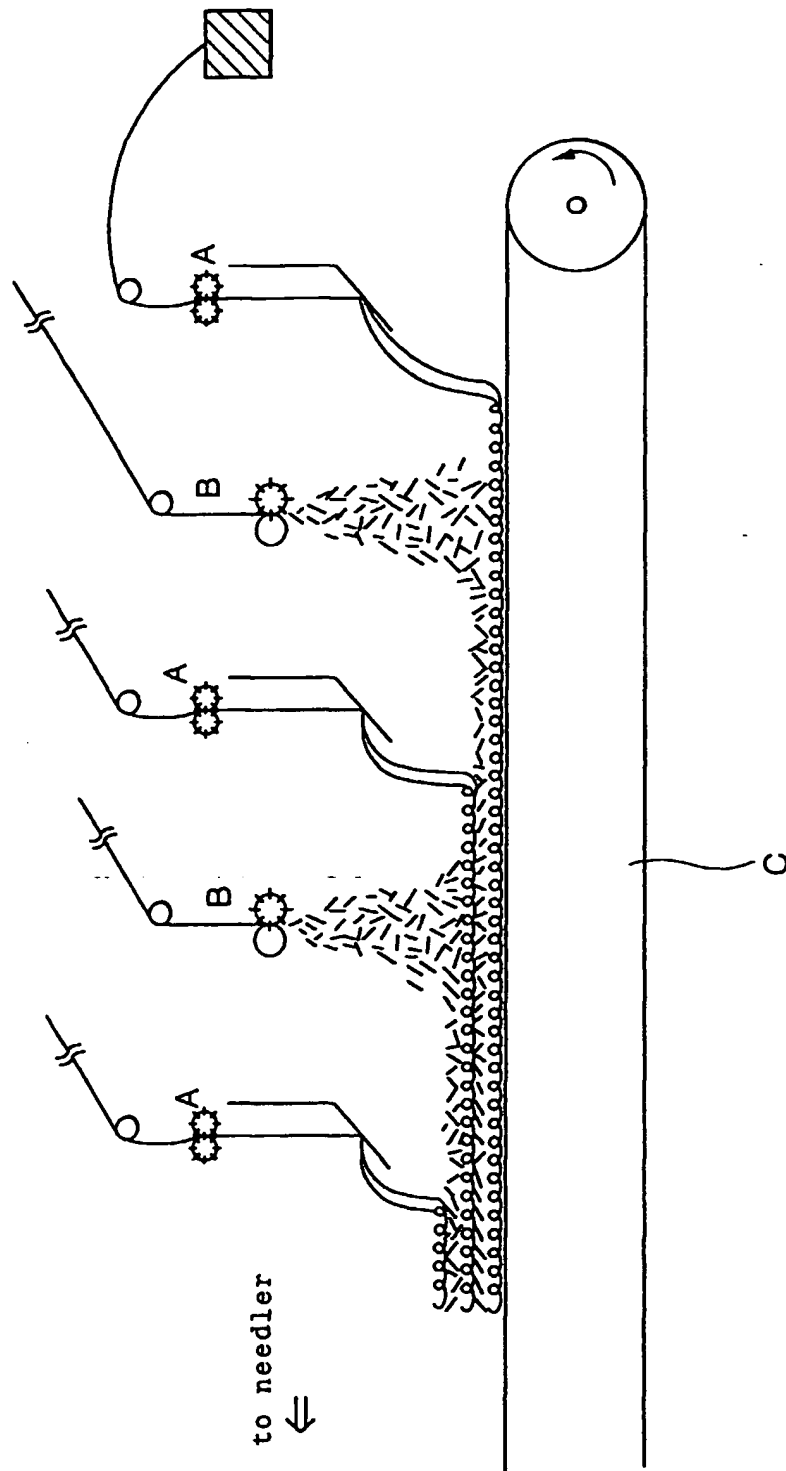


FIG.7



INTERNATIONAL SEARCH REPORT

International application No.

PCT/JP96/01507

A. CLASSIFICATION OF SUBJECT MATTER

Int. Cl⁶ B29B11/16

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

Int. Cl⁶ B29B11/16, B29B15/08-15/14, C08J5/04-5/10, C08J5/24

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Jitsuyo Shinan Koho	1926 - 1996
Kokai Jitsuyo Shinan Koho	1971 - 1996
Toroku Jitsuyo Shinan Koho	1994 - 1996

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	JP, 3-167240, A (Idemitsu Kosan Co., Ltd.), July 19, 1991 (19. 07. 91), Page 1, lower left column, lines 5 to 8; page 7, upper left column, line 3 to upper right column, line 4 & EP, A, 430109	1 - 6
A	JP, 3-167240, A (Idemitsu Kosan Co., Ltd.), July 19, 1991 (19. 07. 91), Page 1, lower left column, lines 5 to 8; page 7, upper left column, line 3 to upper right column, line 4 & EP, A, 430109	7 - 10

☐ Further documents are listed in the continuation of Box C.☐ See patent family annex.

* Special categories of cited documents:

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"A" document member of the same patent family

Date of the actual completion of the international search

August 30, 1996 (30. 08. 96)

Date of mailing of the international search report

September 10, 1996 (10. 09. 96)

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Authorized officer

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